

# Habilitation à diriger les recherches

mention mathématiques et applications

Identification and detection of stochastic systems  
application in structural monitoring

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# Outline

- 1 Subspace identification
  - Consistency of subspace methods
- 2 Damage detection and localization
  - Damage detection
  - Damage localization
- 3 Damage detection and real problems
  - Temperature rejection
  - Flutter detection
- 4 And now ?
  - Damage detection in the frequency domain

# A bit of history

## SISTHEM team past and present

- Past works from M. Basseville, A. Benveniste, M. Goursat
- 1980 - 1991 : Research (4PhD theses)
  - collaboration with IFREMER and EDF
  - BR and IV methods for subspace identification
  - IV damage detection
- 1996-1999 : European project Eureka SINOPSYS :
  - subspace damage detection foundations (Basseville et al.)
  - 1998 : I'm here
- 2000-2008 : new research problems in civil engineering and aircraft monitoring

# Hidden Markov chains

publications from PhD Thesis + postdoc

We will not talk about this.

- 1 Basic properties of the projective product, with application to products of column-allowable nonnegative matrices, Mathematics of Control, Signals and Systems, 2000. with F. LeGland.
- 2 Exponential forgetting and geometric ergodicity in hidden Markov models, Mathematics of Control, Signals and Systems, 2000. with F. LeGland.
- 3 Asymptotical statistics of misspecified hidden Markov models, IEEE Transactions on Automatic Control, 2004. with L. Finesso.

# Applications

Monitoring of integrity and stability

We worked on these structures.



$$\mathbf{M}x''(t) + \mathbf{C}x'(t) + \mathbf{K}x(t) = f(t)$$

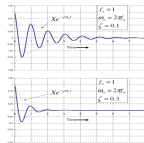
$$\begin{cases} X_{k+1} &= A X_k + V_{k+1} \\ Y_k &= C X_k \end{cases}$$

$$\det(A - \lambda I) = 0, \quad (A - \lambda I) \Phi_\lambda = 0$$

Mechanical engineers talk also about frequency and damping:

$$x(t) = \exp^{\gamma t}, \text{ with } \gamma = \omega(-\zeta \pm \sqrt{\zeta^2 - 1})$$

$$\begin{cases} \omega = \sqrt{k/m} \text{ and } f = \omega / (2 * \pi) \\ \zeta = c / (2 * \sqrt{k * m}) \end{cases}$$



# Why structural health monitoring is important ?

- Civil and aeronautical structures are ageing very fast
- Human inspection is most of the time impractical or non reasonable
- Non all structural behaviour can be predicted by design (e.g. damping)
- Some parameters are critical and need to be monitored (e.g. damping)

# Applications

## context

- Non stationary excitation (turbulence) : unknown, uncontrolled, non measured
- Civil engineering
  - Slow varying structure
  - Large number of sensors
  - Main concern is damage due to ageing
  - Main nuisance is temperature variation
- Aeronautical structures
  - Fast transient structure
  - Large number of modes
  - Main concern is stability and flutter
  - Main nuisance is aeroelasticity interaction



# Identification vs detection

- Identification : what is the system state ?
  - a system is described by a reduced set of features
  - goal : estimate the features.
  - many methods
- Detection : has the system changed ??
  - much simpler goal - provide a simple alarm
  - less precise information on the system state
  - information can be good enough for many applications
- 2 types of structures / 2 types of approaches

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# Subspace identification

## model

$$\begin{cases} x_k = Ax_{k-1} + Bu_k + K(k)\nu_k \\ y_k = Cx_{k-1} + Du_k + L(k)\nu_k \end{cases}$$

where

$$\begin{bmatrix} K(k) \\ L(k) \end{bmatrix} \begin{bmatrix} K^T(k) & L^T(k) \end{bmatrix}$$

is the noise covariance matrix corresponding to the excitation varying in time.

The problem here is the identification of the pair  $(C, A)$ .

# Subspace identification

## model

$$R_i(N) \triangleq \frac{1}{s_N} \langle Y_i, Z_0 \rangle_N \text{ (covariance) or}$$

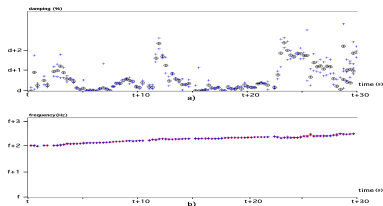
$$R_i(N) \triangleq \frac{1}{s_N} E_N(Y_i | Z_0) \text{ (data driven)}$$

$$\mathcal{H}_p(N) \triangleq \begin{bmatrix} R_1(N) \\ \vdots \\ R_p(N) \end{bmatrix} = \mathcal{O}_p \times G(N) \text{ and } \mathcal{O}_p \triangleq \begin{bmatrix} C \\ \vdots \\ CA^{p-1} \end{bmatrix}$$

- Akaike (1974), Verhaegen (1993), Deistler (1995), Moore (1996), Viberg (1997), Bauer (2000), Ljung (2002), Chiuso (2004), and Benveniste and Fuchs (1985)

# Applications

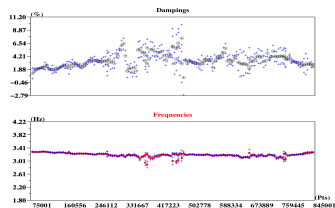
A few examples - monitoring of Ariane 5 booster launch - EADS/CNES



**Figure:** Parameters change during launch period - low uncertainty on frequency - damping is both critical and difficult to estimate

# Applications

A few examples - soccer match in Bradford stadium



**Figure:** Sensors on stadium stand. Monitoring of crowd excitation.  
Jumps in parameter values : goals

# Some output-only subspace algorithms

- Covariance driven subspace identification

$$R_i(N) = \langle Y_i, Z_{0,M} \rangle_N,$$

$$\mathcal{H}_p(N) = \langle \mathcal{Y}_{0,p}^+, \mathcal{Y}_{0,M}^- \rangle_N$$

- Data driven subspace algorithms

$$\mathcal{H}_p(N) = E_N(\mathcal{Y}_{0,p}^+ | \mathcal{Y}_{0,M}^-)$$

$$Z_{0,M} = \begin{bmatrix} Y_0 \\ \vdots \\ Y_{-M} \end{bmatrix}$$

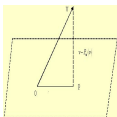
$$\mathcal{Y}_{k,p}^+ = \begin{pmatrix} Y_k \\ \vdots \\ Y_{k+p} \end{pmatrix},$$

$$\mathcal{Y}_{k,p}^- = \begin{pmatrix} Y_k \\ \vdots \\ Y_{k-p} \end{pmatrix}.$$

# Some input/output subspace algorithms

- Using projected past input and output as instruments

$$\mathcal{H}_p = \langle \mathcal{Y}_{0,p}^+, Z_{0,M} \rangle_N,$$



$$Z_i \triangleq E_N \left( W_i \mid \left( \mathcal{U}_{0,M}^+ \right)^\perp \right), \text{ where } W_i \triangleq \begin{bmatrix} U_i \\ Y_i \end{bmatrix}$$

- Using projected inputs as instruments

$$\mathcal{H}_p = E_N(\mathcal{Y}_{0,p}^+ \mid Z_{0,M}),$$

where  $Z_{0,M}$  is defined by  $Z_i \triangleq E_N \left( U_i \mid \left( \mathcal{U}_{0,M}^+ \right)^\perp \right)$

- Many more : CVA, MOESP, N4SID, ...



# Subspace identification and Instruments

"instrument  $z_k$  depends on observable quantities" :

$z_k$  is measurable wrt the  $\sigma$  algebra  $\sigma(u_j : j \in \mathbb{Z}) \vee \sigma(y_l : l \leq k)$

"instrument has sustainable energy" :

$$\lim_{N \rightarrow \infty} s_N = \infty, \text{ where } s_N \triangleq \sum_{k=-M}^{N-1} \|z_k\|^2$$

"instrument is not much correlated to the inputs" :

$$\left\langle \begin{bmatrix} B \\ D \end{bmatrix} u_j, z_0 \right\rangle_N = o(s_N) \text{ for } j > 0$$

"instrument is well correlated to the state" :

$$\liminf_{N \rightarrow \infty} \sigma_n \left( \frac{1}{s_N} \langle X_0, z_0 \rangle_N \right) > 0$$

# Subspace identification

a few comments

- Most subspace methods fit this "instrument" framework
- Non stationary excitation : coherency with applications

## Theorem (consistent estimator)

$(C(N), A(N))$  derived from  $\mathcal{H}_p(N)$  is a consistent estimator of  $(C, A)$

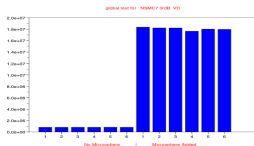
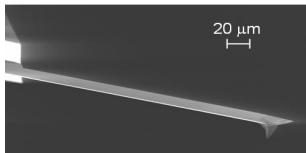
Nonstationary consistency of subspace methods, IEEE Transactions on Automatic Control, 2007.  
with A. Benveniste.

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## A few applications

### nano MEMS particle detection



**Figure:** Mass detection (1 particle nano) on cantilever beam by detection. Repeatability over 6 different nano beams is checked. Collaboration with Purdue University

# Damage detection

## Residual definition

$$E_{\theta} H(\theta_*, Y) = 0 \text{ if } \theta = \theta_*$$

and

$$E_{\theta} H(\theta_*, Y) \neq 0 \text{ if } \theta \neq \theta_*$$

Now define a time-normalized residual

$$\zeta_N(\theta) = \frac{1}{\sqrt{N}} \sum_{t=1}^N H(\theta, Y_t)$$

Detection of Abrupt Changes - Theory and Applications -  
Basseville and Nikiforov (1993).

# Damage detection

## The local approach

$$\theta - \theta_* = \frac{1}{\sqrt{N}} \delta, \text{ with } \delta \text{ independent of } N$$

What it means ??

- In Theory : we can obtain central limit theorems for the "damaged" scenario
- In Practice : the more samples we have, the smallest change we can detect
- With respect to others : it is a simple way to infer about the damaged state, without assuming too much about it

# Damage detection

## Statistical convergence

### Theorem (central limit theorem for local approach)

$$\begin{cases} \zeta_N(\theta_*, \theta) \longrightarrow \mathcal{N}(\mathbf{0}, \Sigma(\theta_*, \theta)) & \text{if } \theta = \theta_* \\ \zeta_N(\theta_*, \theta) \longrightarrow \mathcal{N}(-\mathbf{J}(\theta_*, \theta)\delta, \Sigma(\theta_*, \theta)) & \text{if } \theta = \theta_* + \frac{\delta}{\sqrt{N}} \end{cases}$$

$$\begin{aligned} \mathbf{J}(\theta_*, \theta) &= -\mathbf{E}_\theta \left( \frac{\partial H}{\partial \theta_*}(\theta_*, Y(\theta)) \right) \\ \Sigma(\theta_*, \theta) &= \lim_{N \rightarrow +\infty} \text{Cov}_\theta(\zeta_N(\theta_*, \theta)) \end{aligned}$$

The change detection problem consists in answering the following question: do we still have  $\theta = \theta_*$  ?

This task is achieved by computing the following  $\chi^2$  test

$$\chi^2(\theta_*, \theta) = \bar{\zeta}_N^T(\theta_*, \theta) \mathbf{K}^{-1}(\theta_*, \theta) \bar{\zeta}_N(\theta_*, \theta)$$

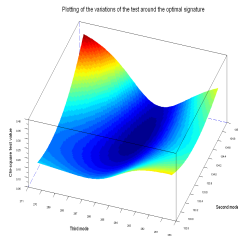
with

$$\bar{\zeta}_N^T(\theta_*, \theta) = \mathbf{J}^T(\theta_*, \theta) \Sigma^{-1}(\theta_*, \theta) \zeta_N(\theta_*, \theta)$$

and the Fisher matrix information as follows

$$\mathbf{K}(\theta_*, \theta) = \mathbf{J}^T(\theta_*, \theta) \Sigma^{-1}(\theta_*, \theta) \mathbf{J}(\theta_*, \theta)$$

Estimation of  $\mathbf{K}$  is a very tricky problem (very slow convergence).





# An application where **K** computation is critical

Painter Street Overstrass - California - collaboration with University of Vancouver, Ca  
and University of Aalborg, DK

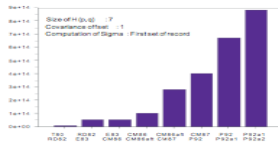
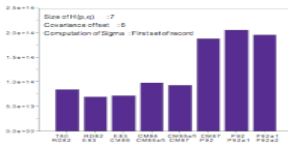


Figure: Damage detection. Very few samples (seismic data) - bootstrap methods.

# Damage detection

## Subspace

$$\zeta_N(\hat{\theta}_*, \theta) = \sqrt{N} \text{vec}(S(\hat{\theta}_*)^T \mathcal{H}_p)$$

$$\left. \begin{array}{l} S(\hat{\theta}_*)^T \mathcal{O}_p(\hat{\theta}_*) = 0 \\ S(\hat{\theta}_*)^T \mathcal{H}_p = 0 \end{array} \right\} \Leftarrow \mathcal{H}_p = \mathcal{H}_p(N) = \mathcal{O}_p(\theta) \times C_p$$

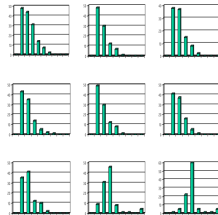
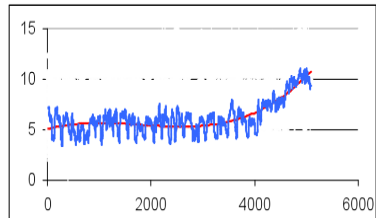
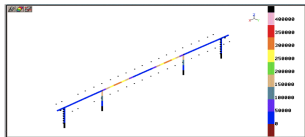
Subspace-based algorithms for structural identification, damage detection, and sensor data fusion, Journal of Applied Signal Processing. with M. Basseville, A. Benveniste, M. Goursat. 2007

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# Damage localization

Bridge Z24. Eureka SINOPSIS project. Collaboration with LMS



# Damage Localization

## A few comments

$$\mathbf{J}(\theta_*, \theta) = -\mathbf{E}_\theta \left( \frac{\partial H}{\partial \theta_*}(\theta_*, Y(\theta)) \right)$$

What it means ??

- The jacobian infers on the sensitivity with respect to any parameterization
- FEM parameterization for localization
- $size(\theta) \approx 100 \ll size(FEM) \approx 20k$

# Damage Localization

A few plots

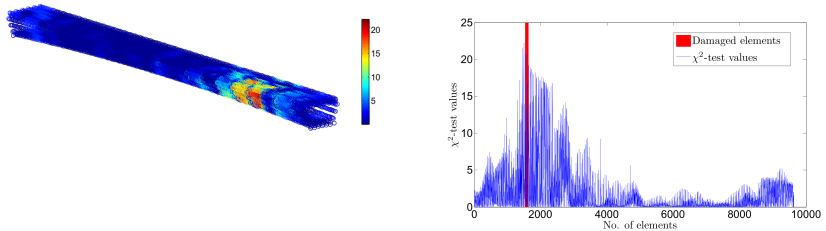


Figure: Damage Localization on bridge deck from ECP.

# ACI CONSTRUCTIF

Collaboration with LCPC/ECP/SDTOOLS and HIT, China

- 1 Statistical model-based damage detection and localization subspace-based residuals and damage-to-noise sensitivity ratios, Journal of Sound and Vibration, 2004.
- 2 Statistical model-based damage localization : a combined subspace-based and substructuring approach, Structural Control and Health Monitoring, 2008.

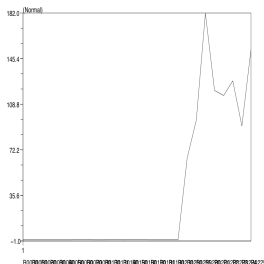
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## A few applications

### Roberval bridge - France



**Figure:** Damage detection on the Roberval bridge - Summer/Winter effect. Collaboration LCPC/KUL

## Temperature modelling

$$M_{\text{struc}}\ddot{X} + C\dot{X} + (K_{\text{struc}} + K_T)X = V$$

$$A = \begin{bmatrix} 0 & I \\ -M_{\text{struc}}^{-1}(K_{\text{struc}} + K_T) & -M_{\text{struc}}^{-1}C \end{bmatrix}$$

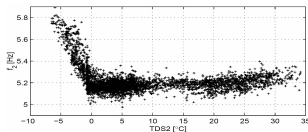


Figure: Frequency evolution on Bridge Z4 (KUL)

if  $T$  changes, reference model is wrong and has to be corrected

# Temperature rejection

## State of Art

- Analytical model based methods  
[Cawley 97],[Moorty 1992]
- Subspace identification (regression ARX)  
[Peeters & De Roeck 2000]
- Factor analysis [Kullaa 2002], modal filters [Deraemaeker & al 2006]
- Subspace detection (database of scenarios # T)  
[Fritzen & al 2003]
- PCA  
[Yan & al, 2004]

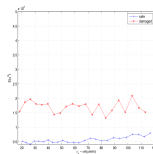
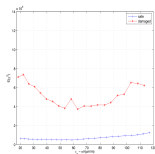
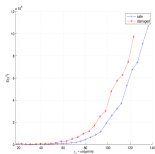
# Temperature rejection

## ACI CONSTRUCTIF - methods of rejection

- Correct the reference model by a thermal model  
 $T \rightarrow (M, K_T) \rightarrow S(\theta_T)$
- Learn the reference by averaging scenarios at different  $T$   
 $\bar{H} = \sum_i H_i \rightarrow S$
- Give the good direction (only works for small changes) :  
Minmax rejection of the temperature as a nuisance  
(skipped in this talk)

# Temperature rejection

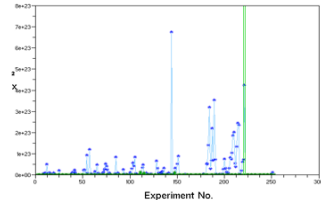
ACI CONSTRUCTIF - LCPC experiment in climate chamber



**Figure:** LCPC beam in climate chamber : 1/ empirical method by merging scenarios 2/ model based correction

# Temperature rejection on civil structures

## Jeronimo church - Portugal



**Figure:** Blue : no temperature rejection. Green : temperature rejection. Green peak : seism detection. Collaboration with Minho University and KUL

# ACI CONSTRUCTIF

Collaboration Ecole Centrale De Paris / LCPC

## PhD Houssein Nasser

- 1 Merging sensor data from multiple temperature scenarios for vibration-based monitoring of civil structures, Structural Health Monitoring, 2008.
- 2 Handling the temperature effect in vibration-based monitoring of civil structures : a combined subspace-based and nuisance rejection approach, Control Engineering Practice, 2008.

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# Flutter detection

Flutter : dynamic aero-elastic instability of a surface exposed to wind

- **Flight Flutter Testing : Design the flutter free flight envelope for ensuring the aircraft stability**  
⇒ Very expensive and time consuming process
- Flutter : loss of stability leads to mechanical wreckage



- Project Eureka Flite and Flite 2 with Onera, Airbus, Dassault Aviation, Sopemea, LMS, VUB and KUL

# Flutter detection

## Aeroelasticity modelling

$$M\ddot{X} + C\dot{X} + KX = U^2DX + UEX + V$$

$$A = \begin{bmatrix} 0 & I \\ -M_{\text{struc}}^{-1}(K_{\text{struc}} - U^2D) & -M_{\text{struc}}^{-1}(C_{\text{struc}} - UE) \end{bmatrix}$$

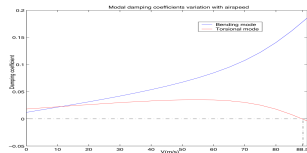
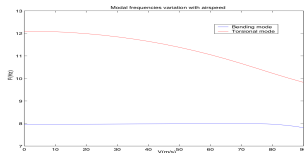


Figure: Frequency and damping evolution

# Flutter detection

## State of art

Current Flutter speed prediction algorithms using vibration data

- damping fit method
- Flutter margin (Zimmerman-Weissenburger)
- envelope function method
- Nissim-Gilyard method
- Flutterometer (Nasa)

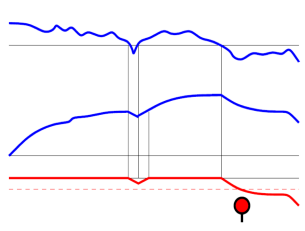
Flutter speed prediction using aerodynamic theory

- numerical fluid-structure interaction algorithms
- the  $k$  method and the  $p - k$  method
- the  $\mu$  method

# Flutter detection

Methodology - R. Zouari - PhD thesis

- Statistical detection - realtime / robust to noise / simple
- Objective : early detection of "flutter"
- CUSUM test built on the foundations of the local approach
- Detect instant of flutter



# Flutter detection

## Cusum algorithm

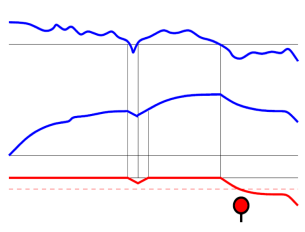
$$\bar{\zeta}_n(\theta_*) \triangleq \mathcal{J}_n(\theta_*, \theta)^T \Sigma_n^{-1}(\theta_*, \theta) \text{vec}(\mathcal{S}(\theta_*)^T \mathbf{1} / n \sum_{i=p}^{n-p} \mathcal{Y}_{i,p}^+ \mathcal{Y}_{i,p}^{-T})$$

$$\mathbf{Z}_n(\theta_*) \triangleq \mathcal{J}_n(\theta_*, \theta)^T \Sigma_n^{-1}(\theta_*, \theta) \text{vec}(\mathcal{S}(\theta_*)^T \mathcal{Y}_{n,p}^+ \mathcal{Y}_{n,p}^{-T})$$

$$R_n(d) \triangleq \sum_k \bar{\Sigma}_k(d)^{-1/2} Z_k(d)$$

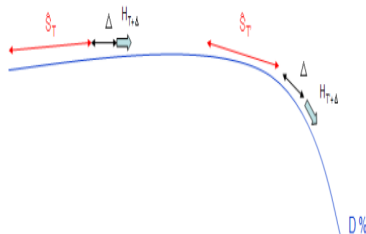
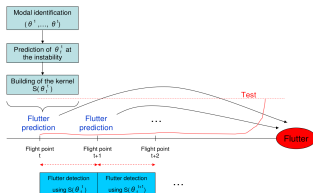
$$T_n(d) \triangleq \max_k R_k(d)$$

$$g_n(d) \triangleq R_n(d) - T_n(d)$$



# Flutter detection

## Model vs Empirical methods - collaboration VUB



- Model : predicted flutter point : combined data/model approach

$$\det(Ms^2 + (C + UB)s + (K + U^2D)) = 0$$

- Empirical : predict instant of critical drop

# Flutter detection

Collaboration ONERA/Airbus/AGH - PoLand

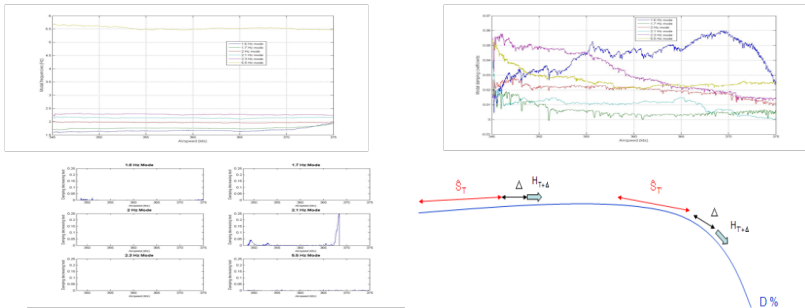


Figure: Simulated two engines aircraft in transient acceleration phase

# Flutter detection

## Flite 1 and Flite 2 projects publications

- 1 Fast in-flight detection of flutter onset : a statistical approach, AIAA Journal of Guidance, Control, and Dynamics, 2005.
- 2 In-flight monitoring of aeronautic structures : vibration-based on-line automated identification versus detection, IEEE Control Systems Magazine, Special Issue on Applications of System Identification, 2007.

### PhD Rafik Zouari

An adaptive statistical approach to flutter detection, in Proceedings of the 17th IFAC World Congress, 2008.



## Comments

- Both problems were approached using some heavy modelling (LCPC/ECP for temperature, VUB for flutter)
- Empirical methods : robust, efficient, automated, black box
- Both problems rely on correcting/adapting the reference / to physical parameter
  - Temperature for civil structure is a nuisance
  - Aeroelasticity for aircrafts is not a nuisance, it has to be detected
- Both problems have different challenges ahead
  - For flutter, aeroelasticity equations can be avoided - just watch the damping drop - but transient effects, system size, turbulence make the problem hard to solve
  - For temperature rejection, the system is quite stationary and small, but the thermal effects are complex - it is not even sure, the assumptions are correct

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# Frequency domain

## Why ?

- A large activity in frequency domain identification
  - Polymax
  - Transmissibility
  - OMAX
  - FDD
- Some advantages for large scale systems
  - Focus on frequency band
  - Not quadratic with sensor
- G. Canales PhD thesis

# Frequency domain

## Polymax - Polyreference LSCF

$$\mathbf{B}(\omega) = \mathbf{H}(\omega)\mathbf{A}(\omega) + \mathbf{V}(\omega), \quad H - H_0 = \frac{1}{\sqrt{K}}\tilde{H},$$

$$\zeta_K^N(\mathbf{B}_{k,0}^N, \mathbf{A}_{k,0}^N, \omega) = \frac{1}{\sqrt{K}} \sum_{k=1}^K (\mathbf{B}_{k,0}^N(\omega) - \mathbf{H}(\omega)\mathbf{A}_{k,0}^N(\omega)) (\mathbf{A}_{k,0}^N(\omega))^H$$

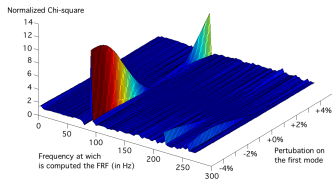
### Theorem (polymax damage detection)

$$\zeta_K^N(\mathbf{B}_{k,0}^N, \mathbf{A}_{k,0}^N, \omega) \sim \mathcal{N} \left( -\tilde{\mathbf{H}}(\omega)\mathbf{S}_0^{aa}(\omega), \mathbf{S}_0^{aa}(\omega)\mathbf{S}_0^{vv}(\omega) \right)$$

$$\chi_K^N(\mathbf{B}_{k,0}^N, \mathbf{A}_{k,0}^N, \omega) = \frac{\zeta_K^N(\mathbf{B}_{k,0}^N, \mathbf{A}_{k,0}^N, \omega) \left( \zeta_K^N(\mathbf{B}_{k,0}^N, \mathbf{A}_{k,0}^N, \omega) \right)^H}{\hat{\mathbf{S}}_0^{aa}(\omega)\hat{\mathbf{S}}_0^{vv}(\omega)}$$

## Frequency domain

Polymax - Polyreference LSCF - Eureka project Flite1



**Figure:** Polyreference LSCF detection on non specified aircraft from an unspecified french aircraft manufacturer

### PhD Gilles Canales

A polyreference least squares complex frequency domain based statistical test for damage detection, in Proceedings of the 17th IFAC World Congress, 2008.

## Discussion

- Identification/Detection : theory AND applications
- Real applications transfer on large scale systems
  - Scilab COSMAD Toolbox used by partners (2001-)
  - identification methods : SNECMA, EADS, ONERA, ...
  - detection methods : LCPC, SVIBS, ...
- Ongoing collaborations
  - academic : KUL, VUB, HIT, UBC, LCPC, ECP, Minho
  - industrial : LMS, SVIBS, SDTOOLS, SNECMA, EADS, ONERA, Dassault

## Discussion

- Past works have focused on
  - time series and subspace methods
  - long stationary sequences
  - small systems
- What has been neglected
  - frequency domain methods
  - confidence intervals and FEM recalage
  - transient events (seismic events and buildings)
  - large systems
- Time of laboratory and academic experiments belong to the past : collaboration with industrials and academic partners is critical

# Real scale implementation

From the bridge Z4 up to now



Figure: Bridge Z24 -1999



Figure: Bridge monitoring project under way funded by Canada government - 2009 - technology transfer - SVIBS DK



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